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## 1. OBJECTIVES

- Investigate the seismic behavior of a steel Concentrically Braced Frame (CBF) using Non-Linear Static Analysis and the Performance-Based Earthquake Engineering
  - Model the structure with the concentrated plasticity approach
  - Highlight the structure main deficiencies
  - Compare them to the actual damages of the structure after the 2011 Tohoku-Oki Earthquake
- Propose seismic retrofit solutions
  - Based on the Capacity Design: New Chevron braces; New X-braces
  - High-performance system: Rocking Braced Frame
- Compare the performance of the retrofit solutions

## 2. STEEL CBF STRUCTURE

- Two-story Parking Garage with CBF structure
  - Columns: HSS 200x200x9, S235
  - Beams:
    - E-W direction: H-350x180x7x11, S235
    - N-S direction: H-450x200x9x14, S235
  - Braces: O-165x6, S275
  - Single-lap gusset plates, creating a 12-mm eccentric load transfer to the braces
  - CBF span length:
    - E-W direction: 4500 mm
    - N-S direction: 7500 mm
- Location
  - Oroshimachi District, Sendai (Japan)

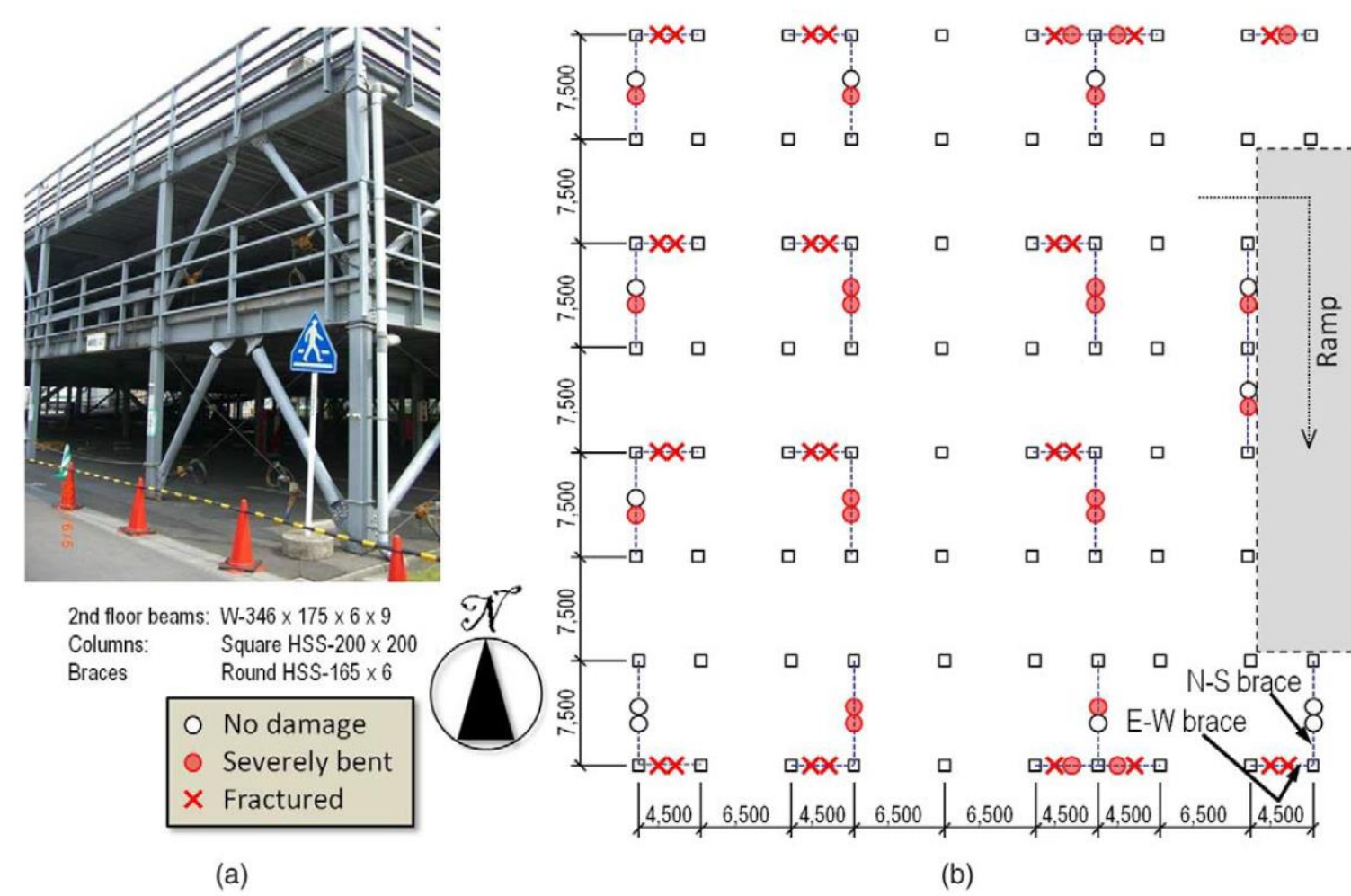


Fig. 1: Parking Garage: (a) Photo; (b) Floor plan

## 3. EARTHQUAKE

- The structure suffered the 2011 Tohoku-Oki Earthquake
  - Magnitude  $M_w$  9.0, 200 seconds long
  - Recorded by station MYG013 of NIED and station N°23 of DCRC within the Oroshimachi District
- Observed Deficiencies after the event
  - Most of the 1<sup>st</sup> story gusset plates fractured in the E-W direction and were severely bent in the N-S direction
  - Plastic Hinge appeared in the beam due to the unbalanced load from the braces
  - Residual drift: 1% in the E-W direction; negligible in the N-S direction



Fig. 2: Fractured Gusset Plates



Fig. 3: Beam deformation

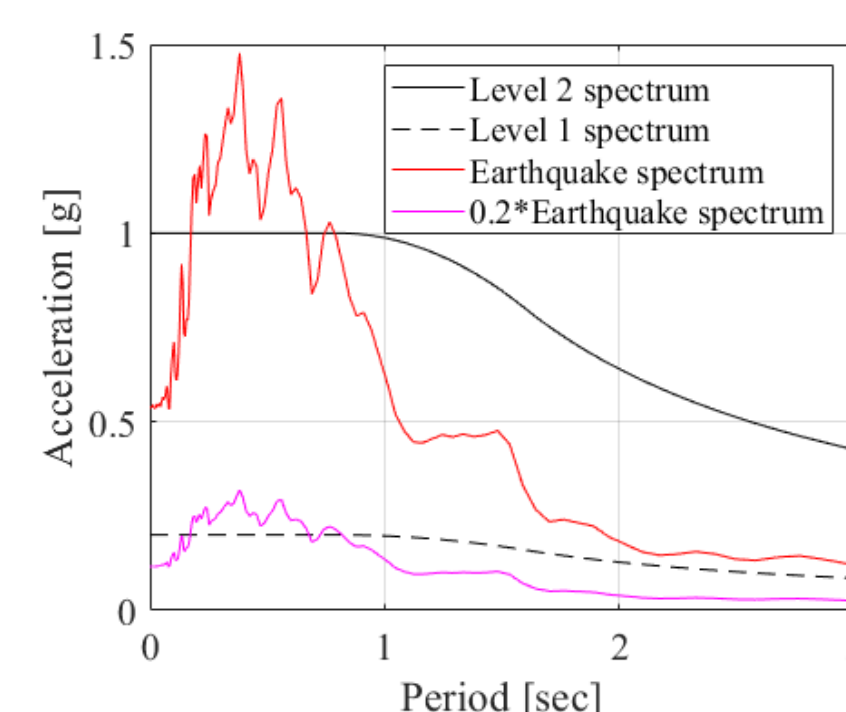


Fig. 4: Spectrum

## 4. NUMERICAL MODEL

- Non-linear model in OpenSees, using the concentrated plasticity approach

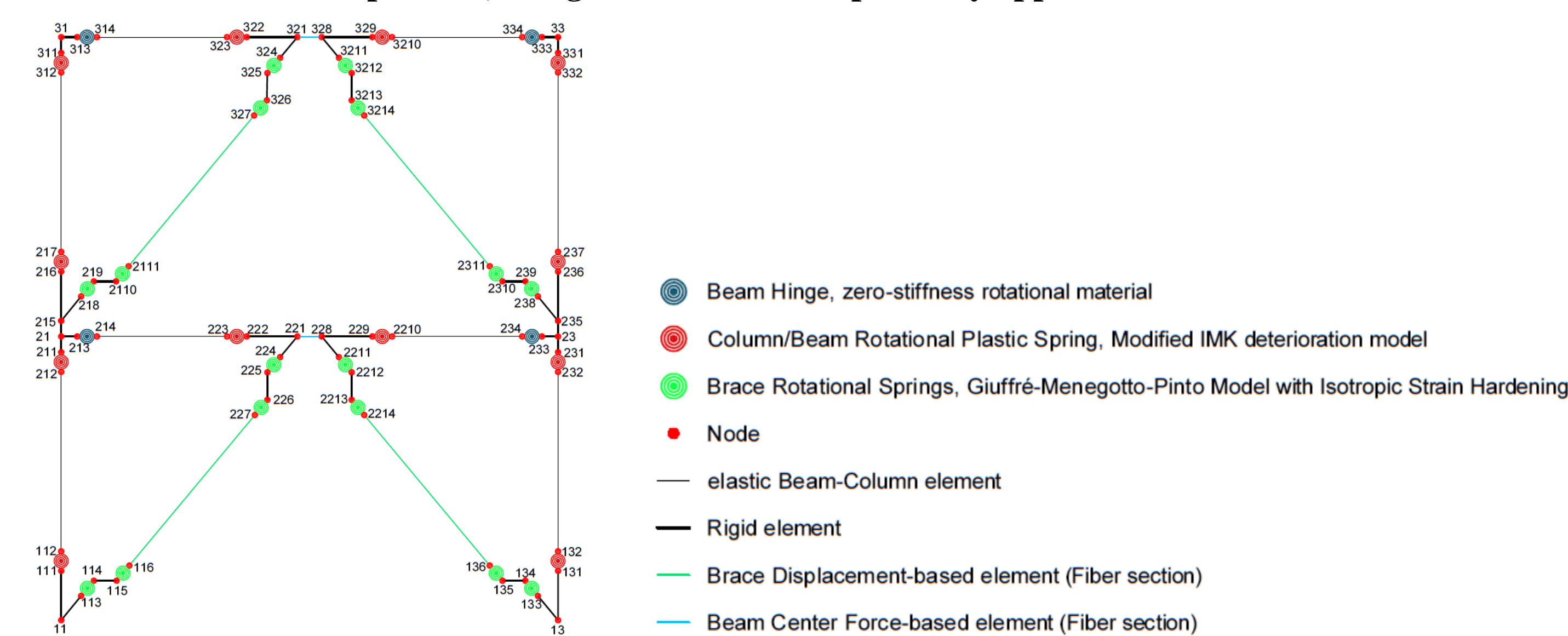


Fig. 5: Model of the initial structure

## 5. NON-LINEAR STATIC ANALYSIS

- The Braces can't develop their buckling and tensile resistance
  - Due to premature fracture of the gusset plates

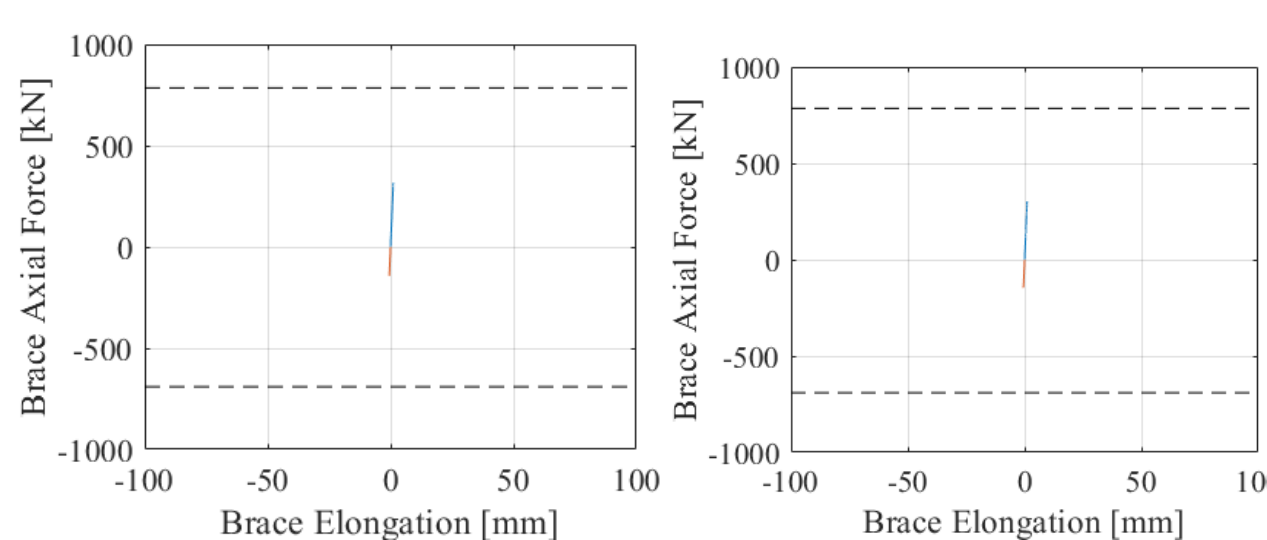


Fig. 6: 1<sup>st</sup> story Braces

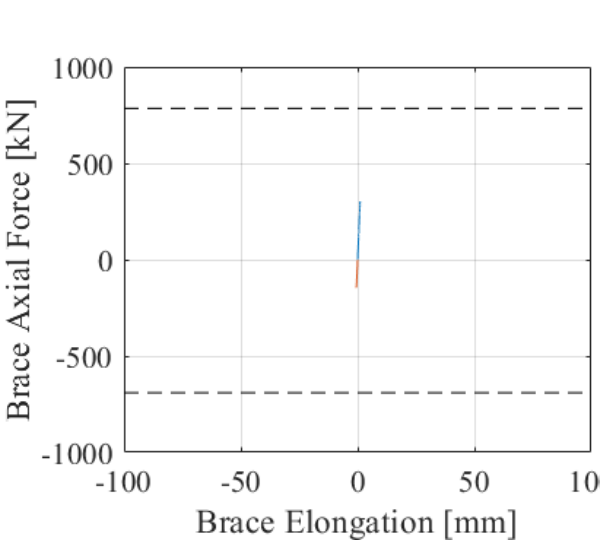


Fig. 7: 2<sup>nd</sup> story Braces

- Assessment according to ASCE/SEI 41-13
  - Target displacement:  $\delta_t = 100$  mm
  - Local Criteria:
    - Braces: do not fulfill any criteria
    - Column rotation: fulfill IO, LS, CP
    - Beam rotation: fulfill IO, LS, CP
- Seismic retrofit is needed

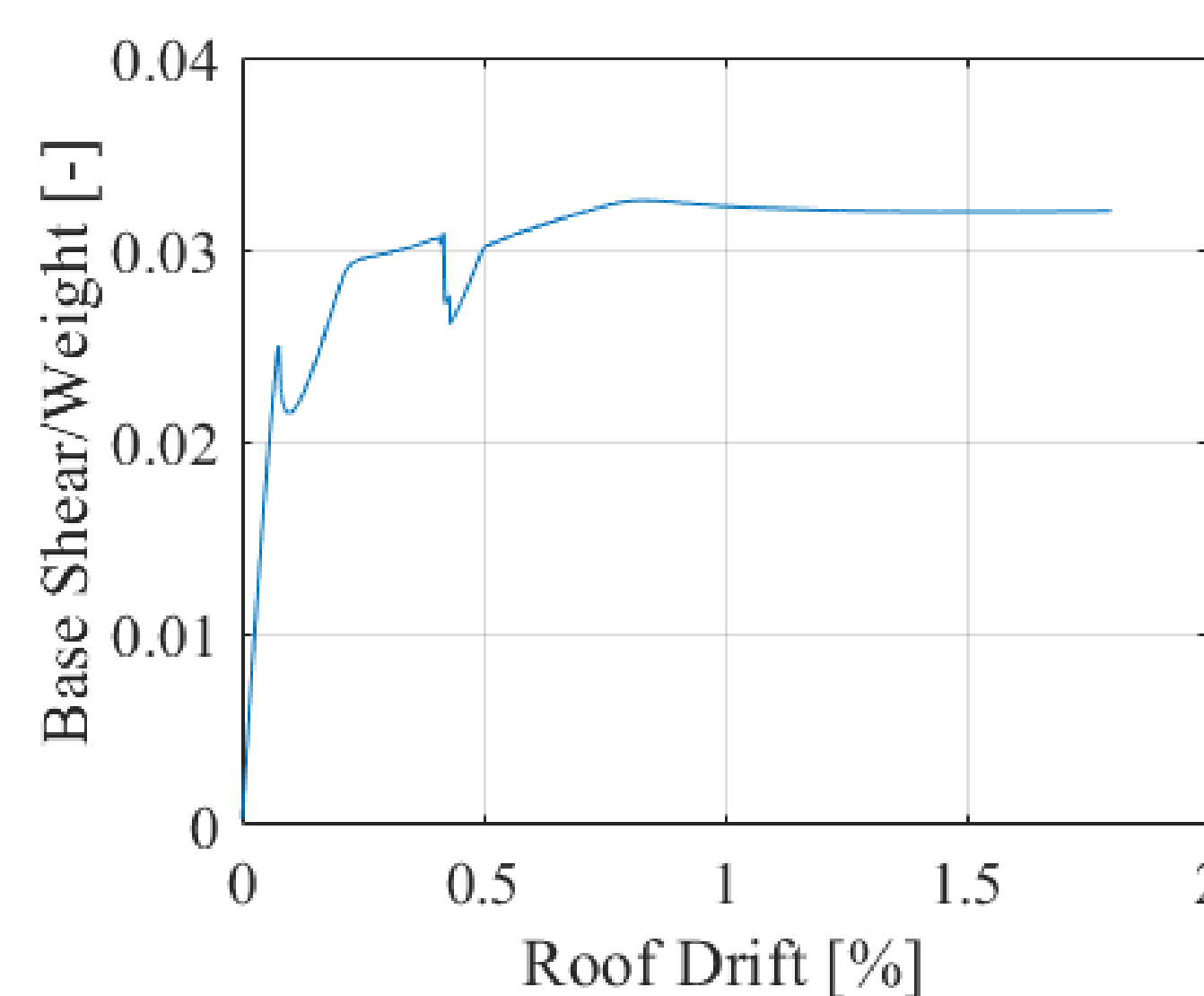


Fig. 8: Global response of the initial structure

## 6. SEISMIC RETROFIT

### 6.1 CONVENTIONAL SEISMIC DESIGN

- New Chevron Braces and Gusset plates

- According to the Capacity Design rules
- 8- $t_{GP}$  elliptical clearance

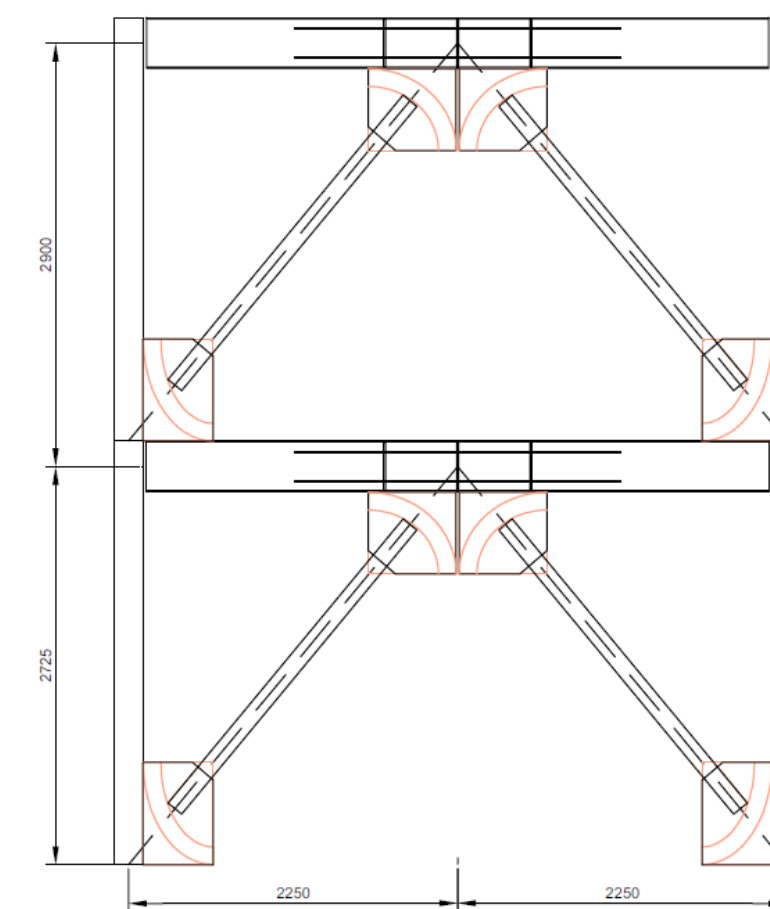


Fig. 9: new Chevron CBF

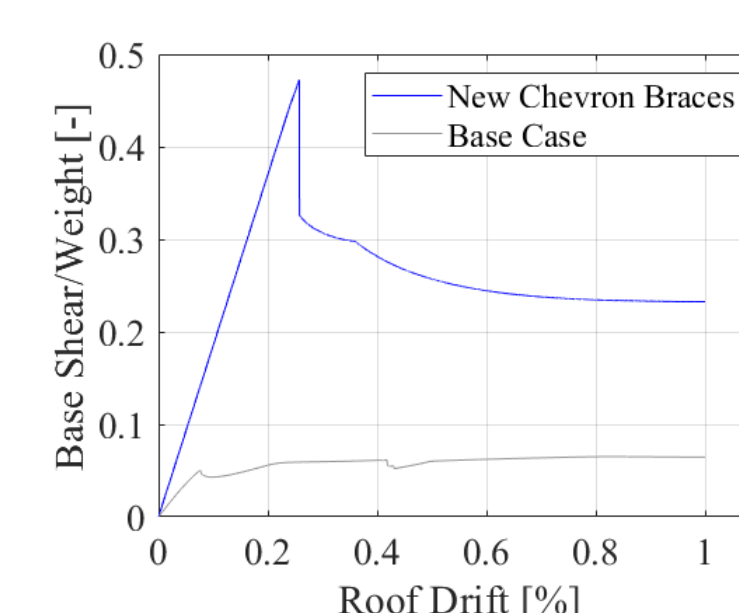


Fig. 11: Global response

- New X-Braces and Gusset plates

- According to the Capacity Design rules
- 8- $t_{GP}$  elliptical clearance

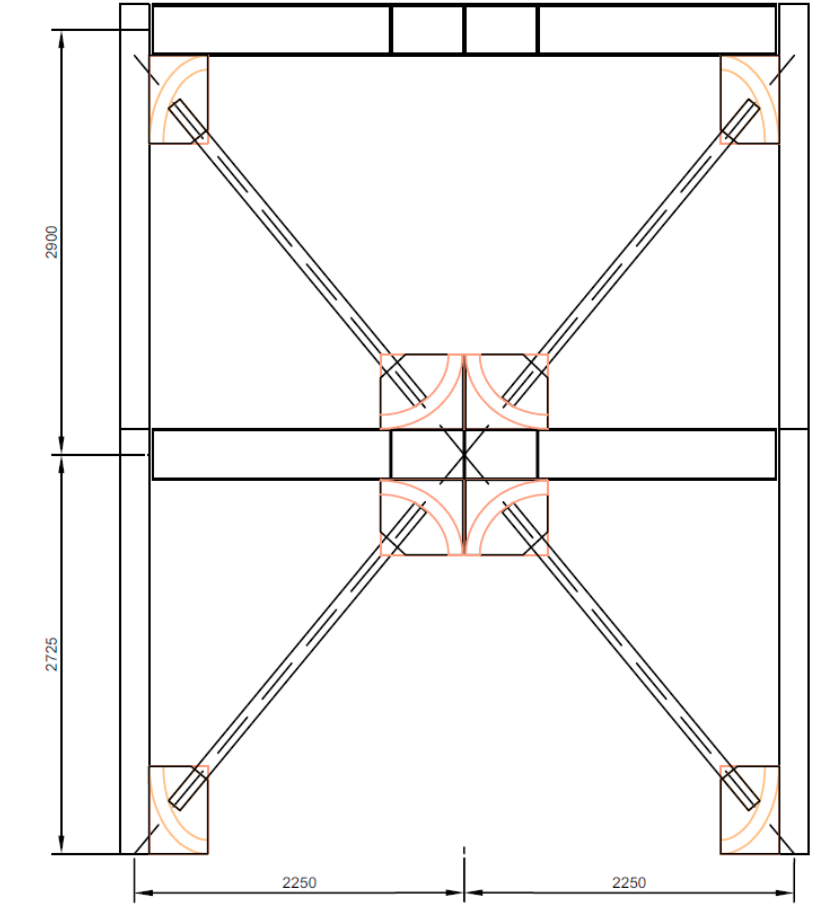


Fig. 10: new X-bracing CBF

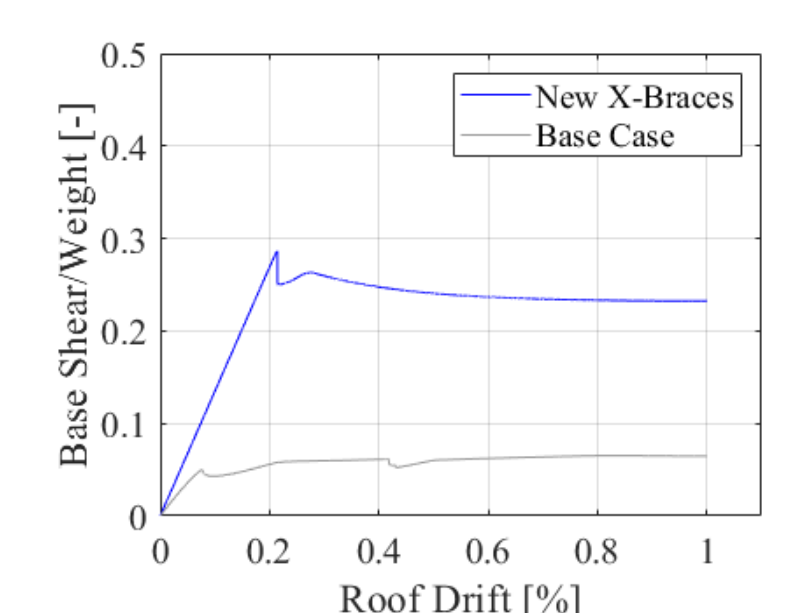


Fig. 12: Global response

- Assessment according to ASCE/SEI 41-13

- Target displacement:  $\delta_t = 8$  mm
- Local Criteria:
  - Braces: fulfill LS, CP
  - Column rotation: fulfill IO, LS, CP
  - Beam rotation: fulfill IO, LS, CP

- Assessment according to ASCE/SEI 41-13

- Target displacement:  $\delta_t = 18$  mm
- Local Criteria:
  - Braces: fulfill LS, CP
  - Column rotation: fulfill IO, LS, CP
  - Beam rotation: fulfill IO, LS, CP

### 6.2 HIGH-PERFORMANCE SYSTEM

- Rocking Braced Frame

- Flag-shaped hysteretic response
- Uplift of the column bases
- Friction energy-dissipating devices
- Needs the strengthening of the gusset plates

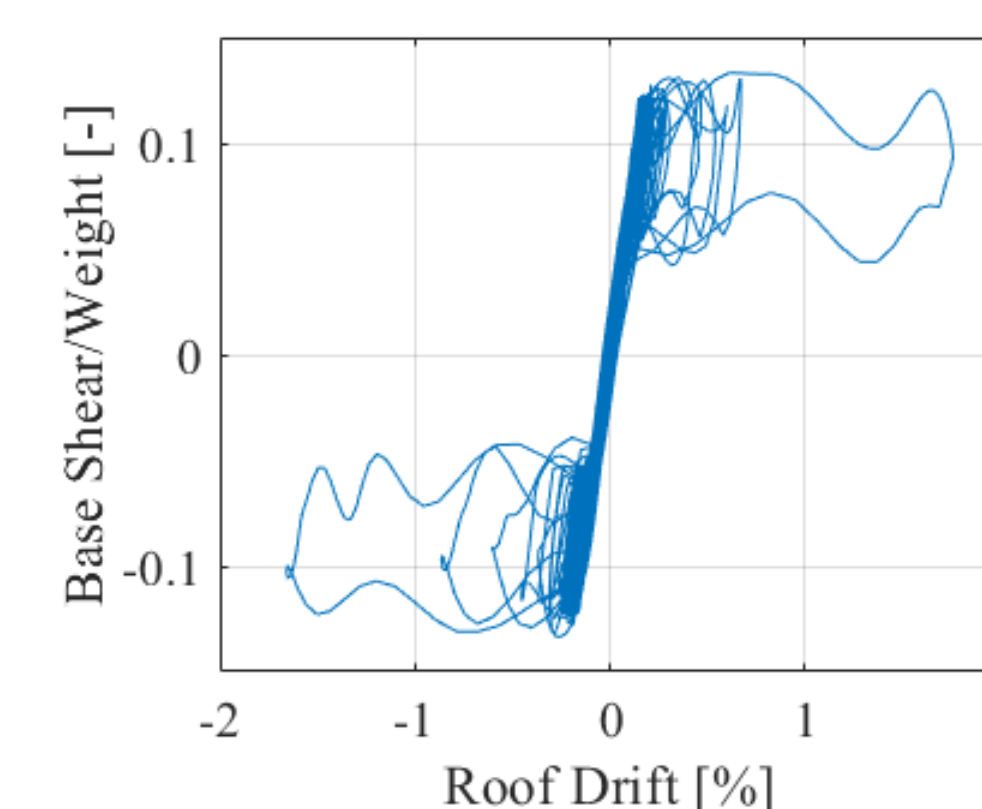


Fig. 13: Global response of the RBF

$F_s = 200$ kN		
Fuse Yield Moment	$M_{fy}$ [kNm]	900
Uplift Moment	$M_{up}$ [kNm]	3060
Flag height	$M_{flag}$ [kNm]	1800
Frame yield moment	$M_y$ [kNm]	3960
Overturning moment	$M_o$ [kNm]	4313
Self-centering	SC [-]	4,53
Global Uplift	UL [-]	4,53
Energy dissipation	ED [-]	23%
Max. Uplift	[mm]	75

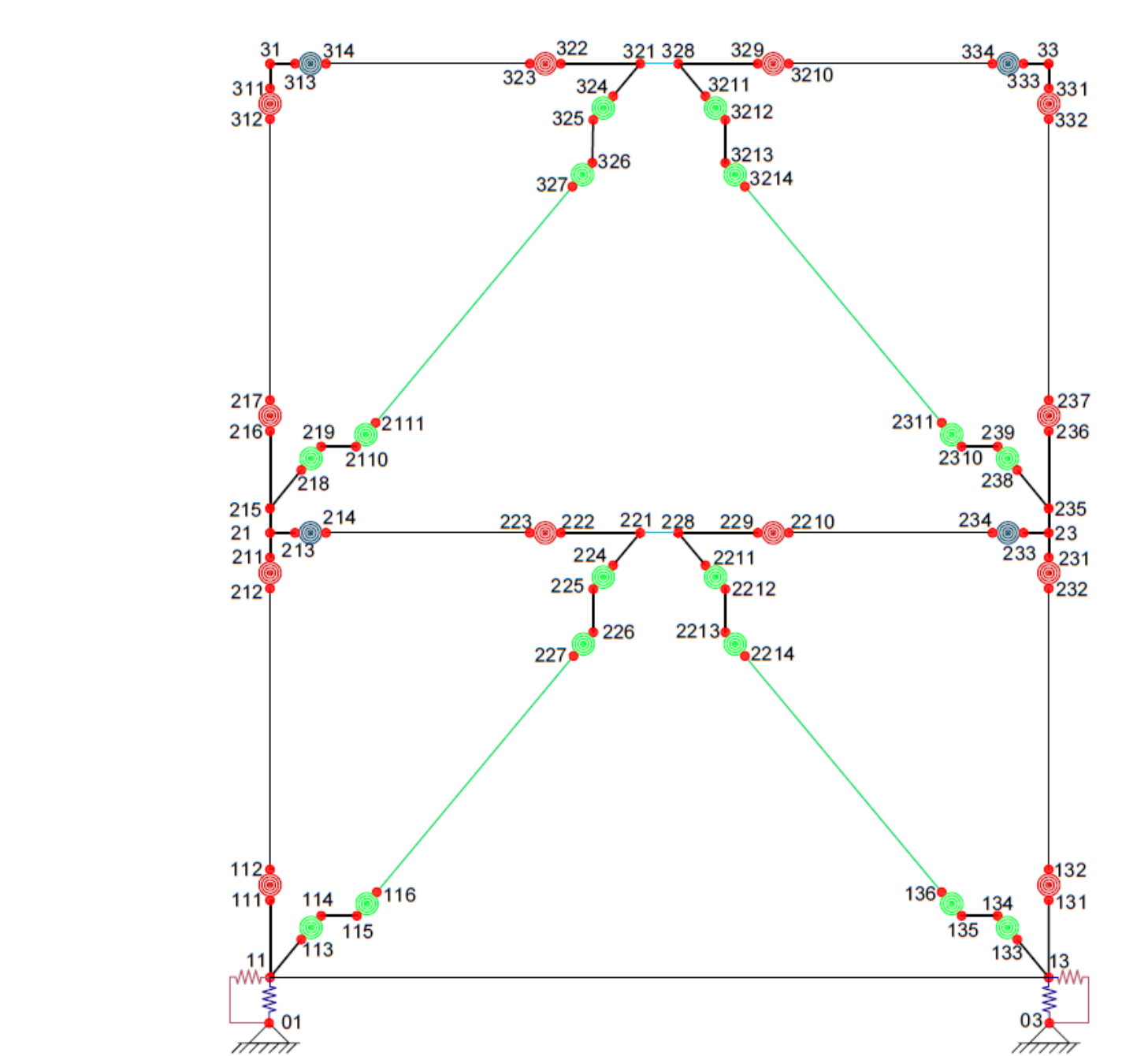


Fig. 14: Model of the RBF

- Beam Hinge, zero-stiffness rotational material
- Column/Beam Rotational Plastic Spring, Modified IMK deterioration model
- Brace Rotational Springs, Giuffrè-Menegotto-Pinto Model with Isotropic Strain Hardening
- Node
- elastic Beam-Column element
- Rigid element
- Brace Displacement-based element (Fiber section)
- Beam Center Force-based element (Fiber section)
- Parallel Vertical Spring : rigid-no tension (ground) + rigid-plastic (fuse) materials
- Horizontal Ground Spring: rigid-no tension material

## 7. NON-LINEAR DYNAMIC ANALYSIS

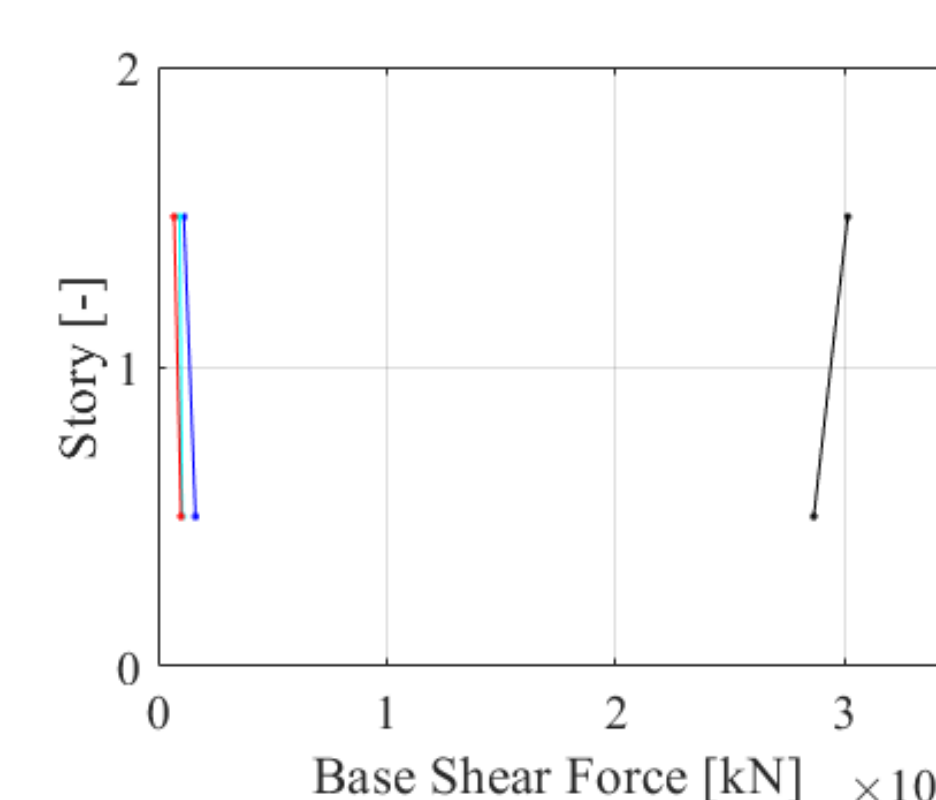


Fig. 14: Maximal Base Shear Force

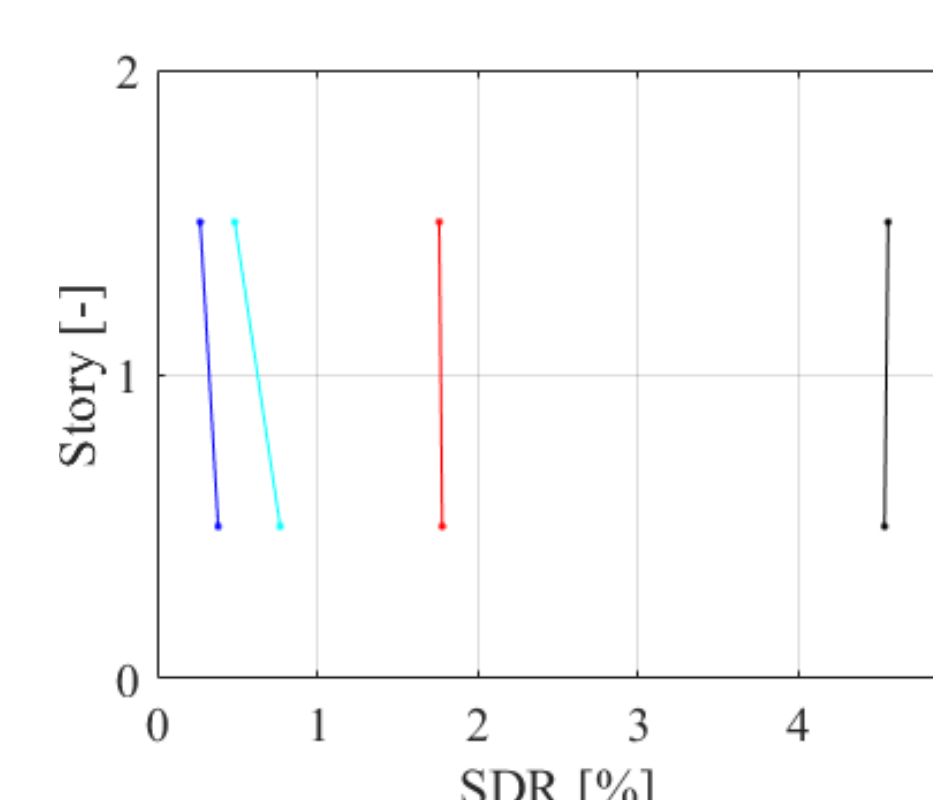


Fig. 15: Maximal Story Drift Ratio

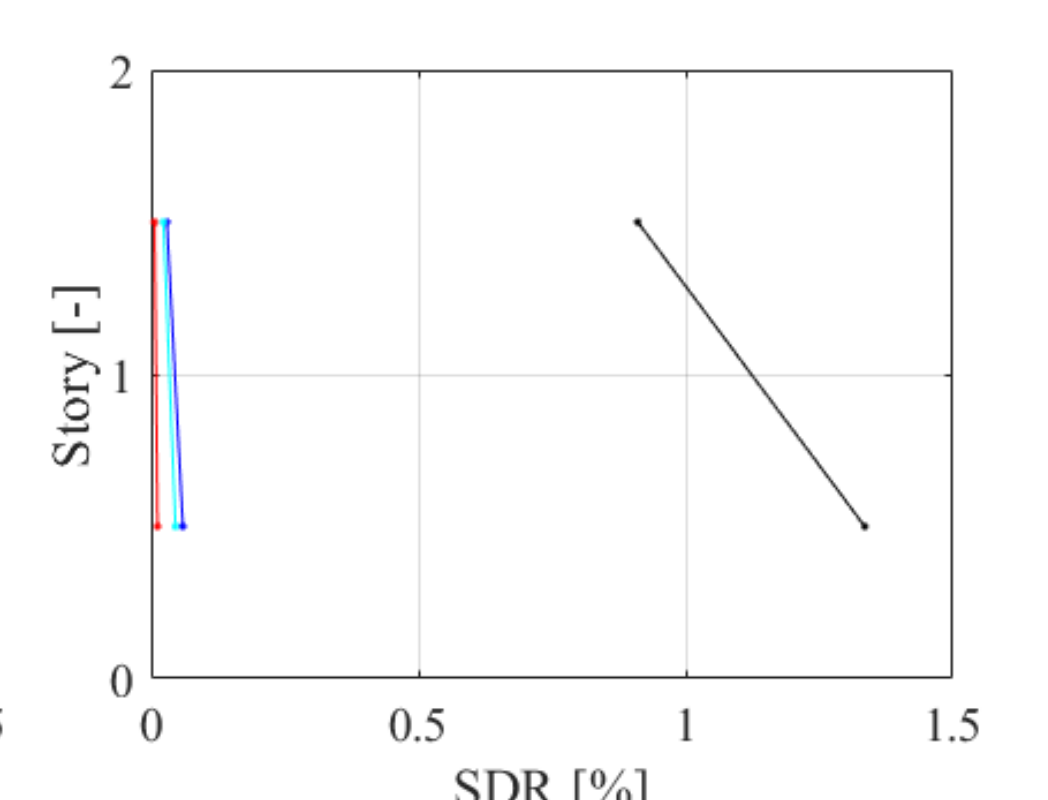


Fig. 16: Residual Story Drift Ratio

- Comparison

- Max. Base Shear Force: Base case > new Chevron Braces > new X Braces > RBF
- Maximal SDR: Base Case > RBF > new X Braces > new Chevron Braces
- Residual SDR: Base Case > new Chevron Braces > new X braces > RBF

- The RBF is the more performing system

- The RBF has the less retrofit effort and less damages after an earthquake